

High-Frequency Filters

(Part 3)

Dr. José Ernesto Rayas-Sánchez

1

Outline

- Richard's transformation
- Example of a low-pass filter using transmission lines
- Kuroda's identities
- Low-pass filter example implemented with microstrips
- Stepped impedance low-pass filters

Richard's Transformation

- It maps ω to Ω , such that we can synthesize inductors and capacitors by using transmission lines

$$\Omega = \tan \beta l = \tan\left(\frac{2\pi}{\lambda} l\right) = \tan\left(\frac{2\pi}{v_p / f} l\right) = \tan\left(\frac{\omega l}{v_p}\right)$$

- The transformation has a period of $\omega l / v_p = \pi$
- Using this new frequency, the reactance of an inductor is

$$jX = j\Omega L = jL \tan(\beta l)$$

and the susceptance of a capacitor is

$$jB = j\Omega C = jC \tan(\beta l)$$

Richard's Transformation (cont.)

- In the Ω domain, an inductor can be replaced with a short-circuited transmission line with characteristic impedance L and electrical length βl :

$$jX = j\Omega L = jL \tan(\beta l) \quad \longrightarrow \quad Z_{\text{in}} = jZ_0 \tan(\beta l)$$

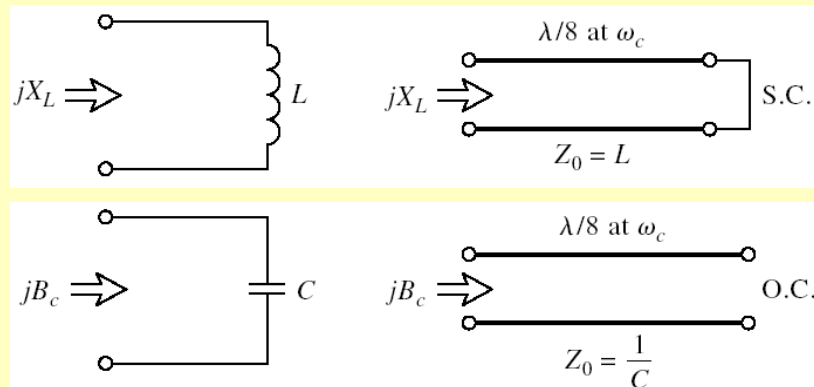
- In the Ω domain, a capacitor can be replaced with an open-circuited transmission line with characteristic admittance C and electrical length βl :

$$jB = j\Omega C = jC \tan(\beta l) \quad \longrightarrow \quad Y_{\text{in}} = j(1/Z_0) \tan(\beta l)$$

Richard's Transformation (cont.)

- Taking $l = \lambda/8$ at f_c ,

$$\Omega = \tan \beta l = \tan \left(\frac{2\pi}{\lambda} \frac{\lambda}{8} \right) = 1 \text{ (normalized frequency)}$$



Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 5

Example: Low-Pass Filter Design

Design a low-pass filter with the following specifications:

- Third-order Chebyshev response with a 3dB ripple level
- Cutoff frequency at 4 GHz
- For a 50- Ω system
- Implemented with transmission lines

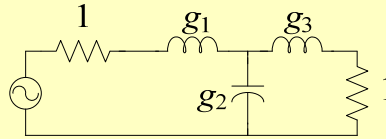
Dr. J. E. Rayas-Sánchez

6

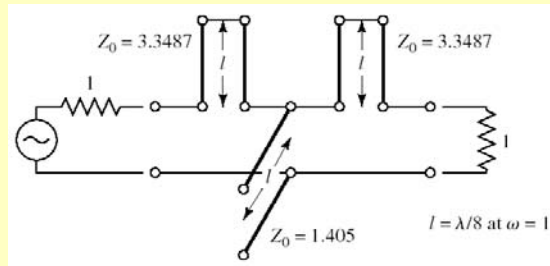
Example: Low-Pass Filter Design (cont.)

From Tables:

$$\begin{aligned} g_0 &= 1 \\ g_1 &= 3.3487 \\ g_2 &= 0.7117 \\ g_3 &= 3.3487 \\ g_4 &= 1 \end{aligned}$$



Using Richard's transformations:



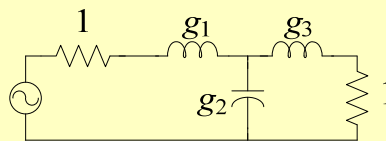
Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 7

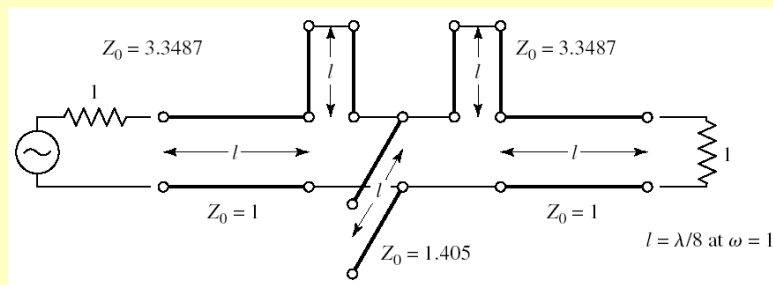
Example: Low-Pass Filter Design (cont)

From Tables:

$$\begin{aligned} g_0 &= 1 \\ g_1 &= 3.3487 \\ g_2 &= 0.7117 \\ g_3 &= 3.3487 \\ g_4 &= 1 \end{aligned}$$



Adding input-output lines:



Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 8

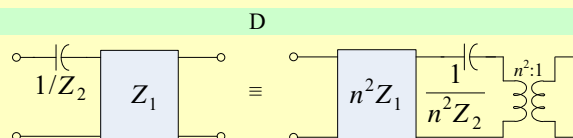
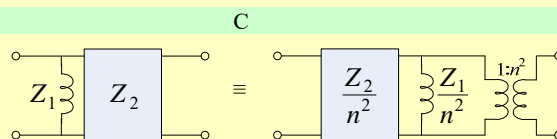
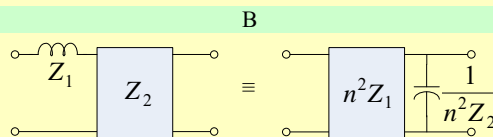
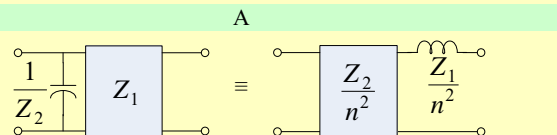
Kuroda's Identities

- They are used to generate more practical filter implementations
- They provide 4 possible transformations
- In the circuits of next slide:
 - Each box represents a transmission line with the indicated characteristic impedance and length $\lambda/8$ at ω_c
 - Each capacitor represents a open-circuited shunt stub of length $\lambda/8$ at ω_c
 - Each inductor represents a short-circuited series stub of length $\lambda/8$ at ω_c

Dr. J. E. Rayas-Sánchez

9

Kuroda's Identities (cont.)



where

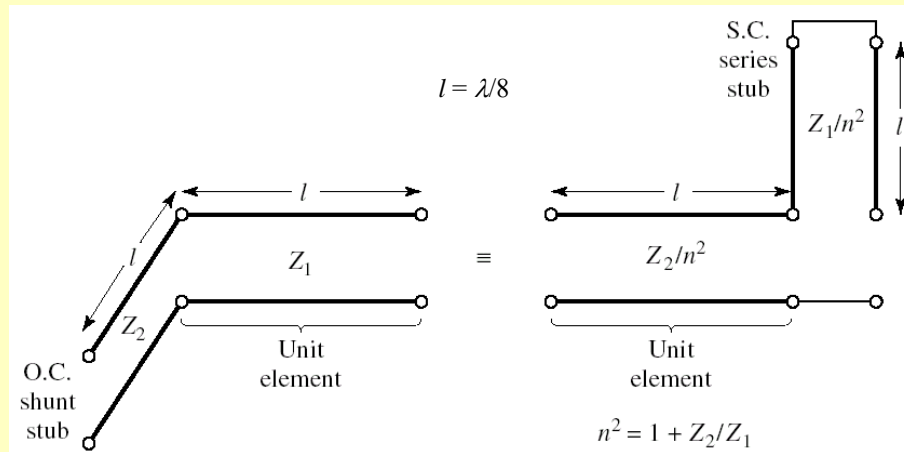
$$n^2 = 1 + \frac{Z_2}{Z_1}$$

Dr. J. E. Rayas-Sánchez

10

Kuroda's Identities (cont.)

Kuroda Identity A

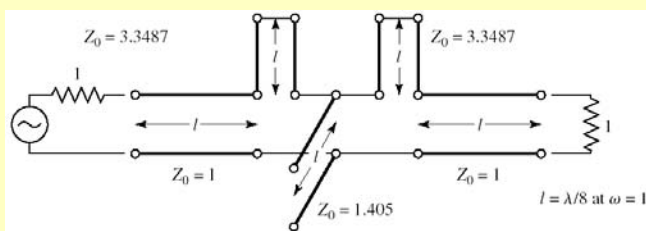


Dr. J. E. Rayas-Sánchez

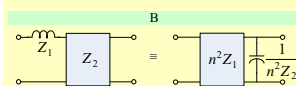
(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 11

Example: Low-Pass Filter Design (cont.)

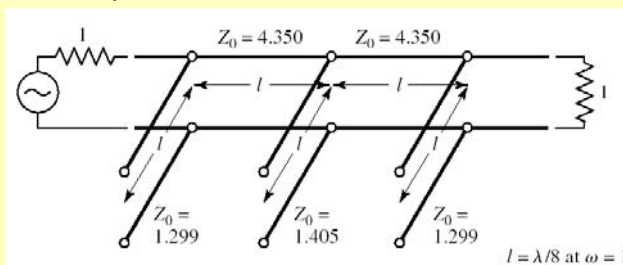
Previous solution:



Applying Kuroda's identity B:



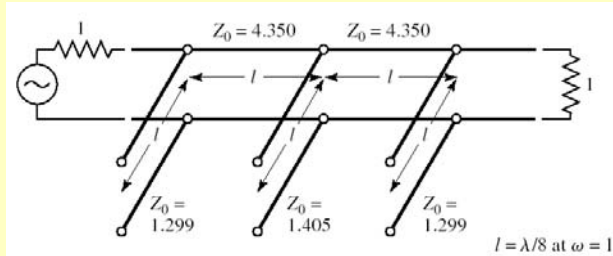
$$\begin{aligned} Z_1 &= 3.3487 ; Z_2 = 1 \\ n^2 &= 1 + Z_2/Z_1 = 1.299 \\ n^2 Z_1 &= 4.35 \\ n^2 Z_2 &= 1.299 \end{aligned}$$



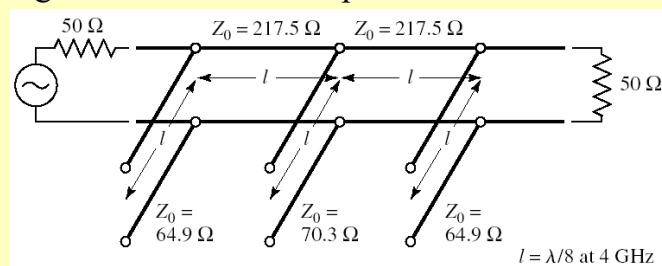
Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 12

Example: Low-Pass Filter Design (cont.)



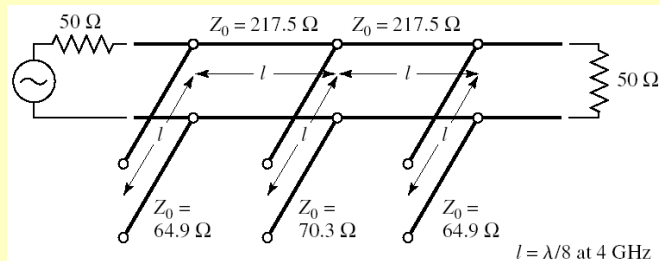
De-scaling the characteristic impedances:



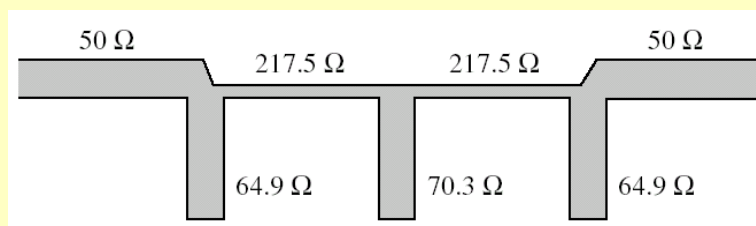
Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) ¹³

Example: Low-Pass Filter Design (cont.)



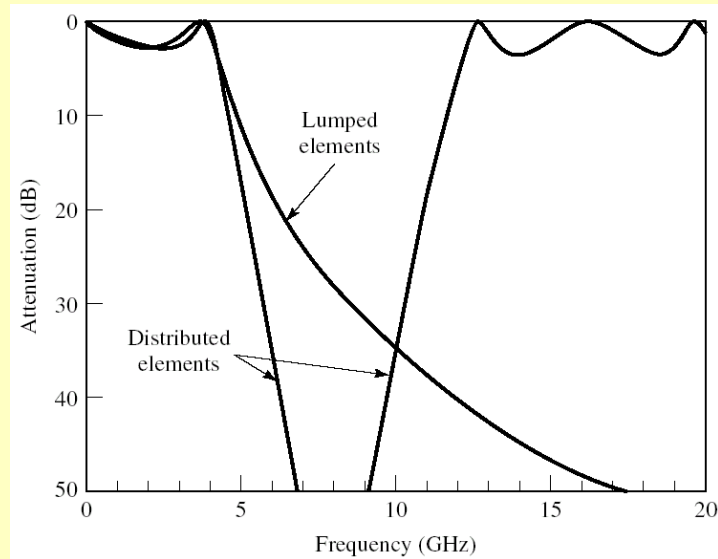
Implementing each transmission line with a microstrip line:



Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) ¹⁴

Example: Low-Pass Filter Design (cont.)



Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 15

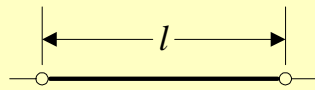
Stepped-Impedance Low-Pass Filters

- They alternate short transmission lines with very high and very low characteristic impedances (HZ-LZ filters)
- They are easier to design and require less area than microstrip implementations using Richard's transformation and Kuroda's identities, but have poorer electrical performance
- They are a very good alternative when a sharp cutoff is not required

Dr. J. E. Rayas-Sánchez

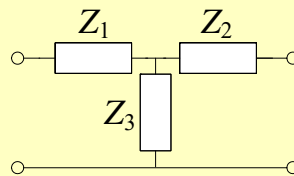
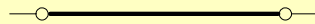
16

From ABCD Parameters...



Z_o, β

$$\begin{aligned} A &= \cos \beta l & B &= jZ_o \sin \beta l \\ C &= jY_o \sin \beta l & D &= \cos \beta l \end{aligned}$$

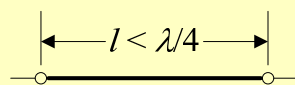


$$\begin{aligned} A &= 1 + \frac{Z_1}{Z_3} & B &= Z_1 + Z_2 + \frac{Z_1 Z_2}{Z_3} \\ C &= \frac{1}{Z_3} & D &= 1 + \frac{Z_2}{Z_3} \end{aligned}$$

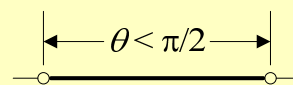
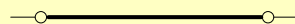
Dr. J. E. Rayas-Sánchez

17

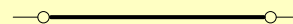
Approximating Short Transmission Lines



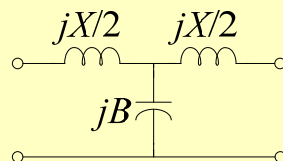
Z_o, β



Z_o, β



Can be approximated by



where

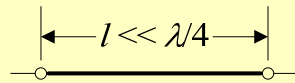
$$X/2 = Z_o \tan(\beta l / 2)$$

$$B = Y_o \sin(\beta l)$$

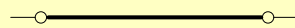
Dr. J. E. Rayas-Sánchez

18

Approximating Short Transmission Lines (cont.)

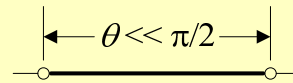
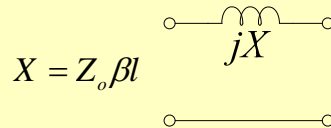


$$Z_o, \beta$$

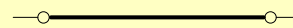


Can be approximated by

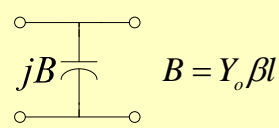
if Z_o is very high,



$$Z_o, \beta$$



if Z_o is very low,



Stepped-Impedance LP Filter – Implementation

- Series inductors are replaced by high-impedance transmission lines (Z_{high})
- Parallel capacitors are replaced by low-impedance transmission lines (Z_{low})
- Lengths of the transmission line sections are calculated using:

$$\beta l_k = \frac{g_k R_0}{Z_{\text{high}}} \quad (g_k \text{ corresponds to an inductor})$$

$$\beta l_k = \frac{g_k Z_{\text{low}}}{R_0} \quad (g_k \text{ corresponds to a capacitor})$$

Stepped-Impedance LP Filter – Example

Design a low-pass stepped impedance microstrip filter with the following specifications:

- Maximally flat response
- $IL_{\min} = 20$ dB at 3.8 GHz
- Cutoff frequency at 2.5 GHz
- For a $50\text{-}\Omega$ system
- Highest practical impedance is $150\text{ }\Omega$, and lowest is $10\text{ }\Omega$

Dr. J. E. Rayas-Sánchez

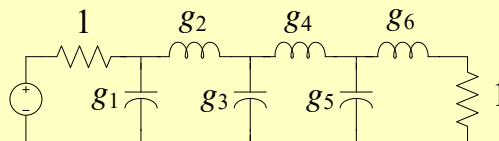
(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 21

Stepped-Impedance LP Filter – Example (cont.)

$IL_{\min} = 20$ dB at 3.8 GHz requires $N = 6$

From Tables:

$$\begin{aligned} g_0 &= 1 \\ g_1 &= 0.5176 \\ g_2 &= 1.4142 \\ g_3 &= 1.9318 \\ g_4 &= 1.9318 \\ g_5 &= 1.4142 \\ g_6 &= 0.5176 \\ g_7 &= 1 \end{aligned}$$

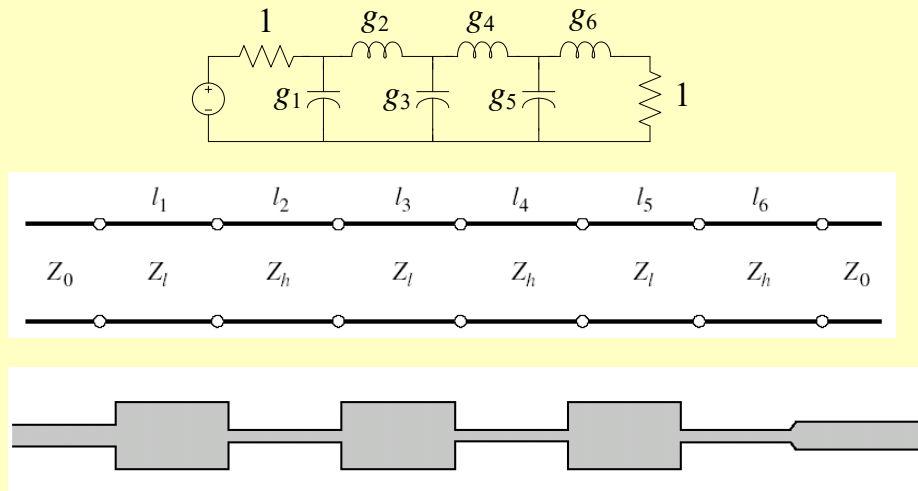


Dr. J. E. Rayas-Sánchez

22

Stepped-Impedance LP Filter – Example (cont.)

Implementation:

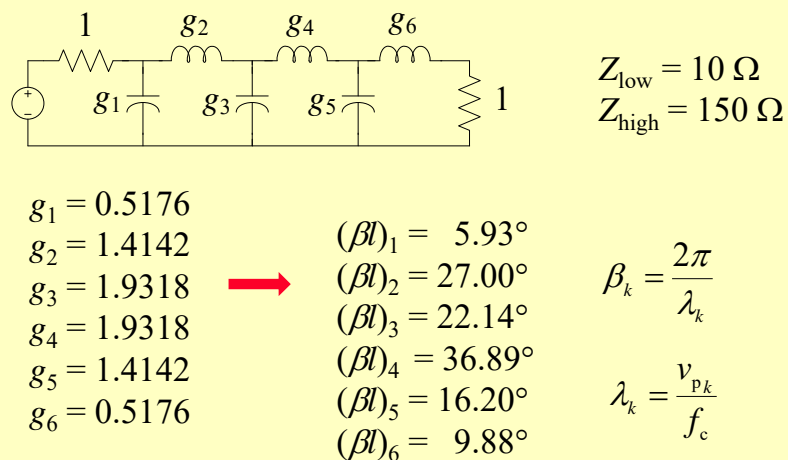


Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) ²³

Stepped-Impedance LP Filter – Example (cont.)

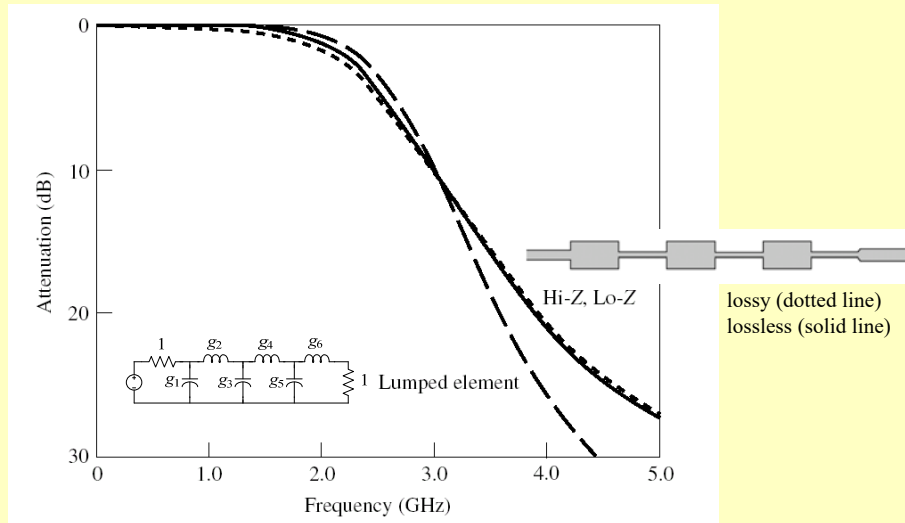
Calculating transmission line lengths:



Dr. J. E. Rayas-Sánchez

24

Stepped-Impedance LP Filter – Example (cont.)



Dr. J. E. Rayas-Sánchez

(D. M. Pozar, *Microwave Engineering*, Wiley, 2005) 25