

FET Fundamental Amplifier Configurations

Dr. José Ernesto Rayas Sánchez

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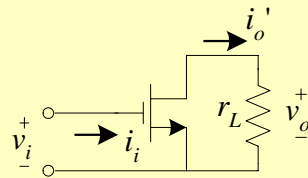
Outline

- Small-signal middle-frequency equivalent circuits
- Common Source (CS)
- Common Gate (CG)
- Common Drain (CD)
- Source Degeneration (SD)
- Comparison between CS, CG, CD and SD
- Distortion limits (dynamic range)

Small-Signal Mid-Frequency Equivalent Circuits

- To analyze an amplifier:
 1. Calculate the DC operating point (bias circuit)
 2. Obtain the small-signal equivalent circuit at medium frequencies
 3. Identify the amplifier's configuration (CS, CG, etc.)
 4. Analyze the small-signal equivalent circuit, either by using formulas or by deriving them

Common Source (CS)



$$A_v = -g_m (r_o \parallel r_L) \quad R_i = \infty \quad R_o = r_o \quad A_i = \infty$$

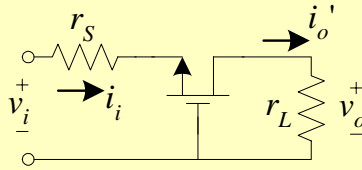
$$\text{If } r_L \ll r_o, \quad A_v = -g_m r_L$$

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Common Gate (CG)



$$A_v = \frac{(1 + g_m r_o) r_L}{r_o + r_S(1 + g_m r_o) + r_L} \approx \frac{g_m r_L r_o}{r_L + r_o(1 + g_m r_S)}$$

$$R_i = r_S + \frac{1}{g_m} \left(1 + \frac{r_L}{r_o} \right) \quad R_o = r_S + r_o(1 + g_m r_S) \quad A_i = 1$$

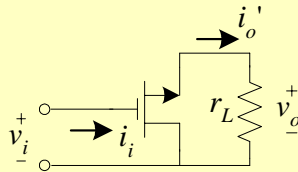
$$\text{If } r_L \ll r_o, \quad A_v = \frac{g_m r_L}{1 + g_m r_S} \quad R_i = r_S + \frac{1}{g_m}$$

$$\text{If } g_m r_S \ll 1, \quad A_v \approx g_m (r_L \parallel r_o) \quad R_o \approx r_o$$

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Common Drain (CD)



$$A_v = \frac{g_m (r_o \parallel r_L)}{1 + g_m (r_o \parallel r_L)} \quad R_i \approx \infty \quad A_i = \infty$$

$$R_o = r_o \parallel \frac{1}{g_m} \approx \frac{1}{g_m}$$

$$\text{If } r_L \ll r_o, \quad A_v \approx \frac{g_m r_L}{1 + g_m r_L} \quad \text{If } g_m r_L \gg 1, \quad A_v \approx 1$$

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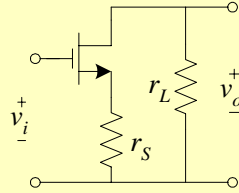
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Source Degeneration (SD)



$$A_v = \frac{-g_m r_o r_L}{r_L + r_S(1 + g_m r_o) + r_o} \quad \text{If } g_m r_o \gg 1, \quad A_v = \frac{-g_m r_o r_L}{r_L + r_o(1 + g_m r_S)}$$

$$\text{If } r_o(1 + g_m r_S) \gg r_L, \quad A_v \approx \frac{-g_m r_L}{1 + g_m r_S} \quad \text{If } g_m r_S \gg 1, \quad A_v \approx -r_L / r_S$$

$$R_o \approx r_S + r_o(1 + g_m r_S) \approx r_o(1 + g_m r_S)$$

$$R_i = \infty \quad A_i \approx \infty$$

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Simplified Formulas – Comparison

	CS	CG	CD	SD
A_v	$-g_m(r_o \parallel r_L)$	$\frac{g_m r_L}{1 + g_m r_S}$	$\frac{g_m r_L}{1 + g_m r_L}$	$\frac{-g_m r_L}{1 + g_m r_S}$
R_i	∞	$r_S + \frac{1}{g_m} \left(1 + \frac{r_L}{r_o}\right)$	∞	∞
R_o	r_o	$r_o(1 + g_m r_S)$	$r_o \parallel \frac{1}{g_m}$	$r_S + r_o(1 + g_m r_S)$
A_i	∞	1	∞	∞

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Over Simplified Formulas – Summary

	CS	CG	CD	SD
A_v	$-g_m r_L$	$g_m r_L$	1	$\frac{-r_L}{r_S}$
R_i	∞	$r_S + \frac{1}{g_m}$	∞	∞
R_o	r_o	r_o	$\frac{1}{g_m}$	$r_o(1 + g_m r_S)$
A_i	∞	1	∞	∞

Distortion Limits

- Distortion limits refer to the maximum output voltage swing for a linear operation (dynamic range)
- They depend on the amplifier configuration, the bias point, and the load line
- For CS amplifiers: $DL^+ = I_{DQ} r_L$ $DL^- = V_{DSQ} - V_{OH}$
- For CD amplifiers: $DL^+ = V_{DSQ} - V_{OH}$ $DL^- = I_{DQ} r_L$
- For CG amplifiers: $DL^+ = I_{DQ} r_L$ $DL^- = V_{DGQ} - V_{OH} + V_{GS}$
- For SD amplifiers: $DL^+ = I_{DQ} r_L$ $DL^- = (V_{DSQ} - V_{OH}) \frac{r_L}{r_L + r_S}$