

# **Modeling Sensors and other Physical Systems with SPICE**

(Part 1)

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## **Simulation of Sensors and Transducers**

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- Sensors, transducers, and other multi-physical components can be simulated in SPICE
- SPICE models for those components are based on:

Analytical functions

Multidimensional vector functions

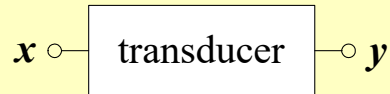
Nonlinear systems of equations

Systems of nonlinear differential equations

Measurements

## Multidimensional Vector Functions

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$\mathbf{x}$  Vector of physical variables (temperature, humidity, pressure, volumetric flow, etc.)

$\mathbf{y}$  Vector of electrical outputs (voltage, current, charge, resistance, etc.)

$$\mathbf{y} = \mathbf{f}(\mathbf{x}) \quad \mathbf{f} : \mathbb{R}^n \rightarrow \mathbb{R}^m$$

It is implemented in SPICE by using controlled sources and independent sources (*R. Saleh and A. Yang, 1993*)

## Implementing $\mathbf{y} = \mathbf{f}(\mathbf{x})$ with SPICE

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- 1) Implement each physical variable,  $x_1, \dots, x_n$  with a DC voltage source, isolated from the rest of the circuit
- 2) Implement each constant or any other parameter using also an isolated DC voltage source
- 3) Use a controlled source to implement each function  $f_1, \dots, f_m$ , using linear controlled sources, polynomial controlled sources, or nonlinear controlled sources

## Linear Controlled Sources

- Types:  $i = gv_c$ ,  $v = ev_c$ ,  $i = fi_c$ ,  $v = hi_c$   
where  $g, e, f, y h$  are real constants,  $v_c$  and  $i_c$  are the controlling signals
- Syntax  
GXXXXXXX N+ N- NC+ NC- VALUE  
EXXXXXXX N+ N- NC+ NC- VALUE  
FXXXXXXX N+ N- VNAME VALUE  
HXXXXXXX N+ N- VNAME VALUE  
(VNAME is the name of the voltage source by which the controlling current is flowing)

## Examples of Linear Controlled Sources

$E1 = v_{5-3} = 3v_{11}$   
E1 5 3 11 0 3.0

$G2 = i_{1-0} = 0.5 \times 10^{-3} v_5$   
G2 1 0 5 0 0.5MMHO

$Hfvcc = v_{8-15} = 900i_{Vmedir}$   
Hfvcc 8 15 Vmedir 0.9K

$F1 = i_{7-51} = 10i_{Vsens}$   
F1 7 51 VSENS 10

## Polynomial Controlled Sources

- Types:  $i = g(v_c)$ ,  $v = e(v_c)$ ,  $i = f(i_c)$ ,  $v = h(i_c)$   
where  $g, e, f, y h$  are polynomial functions of one or more variables, and  $v_c, i_c$  are the controlling signals

- Syntax

```
GXXXXXXX N+ N- <POLY (ND)> NC1+ NC1- ... p0 <p1 ...> <IC=...>
EXXXXXXX N+ N- <POLY (ND)> NC1+ NC1- ... p0 <p1 ...> <IC=...>
FXXXXXXX N+ N- <POLY (ND)> VN1 <VN2 ...> p0 <p1 ...> <IC=...>
HXXXXXXX N+ N- <POLY (ND)> VN1 <VN2 ...> p0 <p1 ...> <IC=...>
```

(VN1, VN2, ... are the names of the voltage sources through which the controlling currents are flowing, ND is the polynomial dimension, IC are the initial conditions)

## Polynomial Controlled Sources (cont.)

Interpretation of polynomial coefficients (p0, p1, ...)

- If ND = 1

$$y = p_0 + (p_1 * a) + (p_2 * a^{**2}) + (p_3 * a^{**3}) + (p_4 * a^{**4}) + (p_5 * a^{**5}) + \dots$$

- If ND = 2

$$y = p_0 + (p_1 * a) + (p_2 * b) + (p_3 * a^{**2}) + (p_4 * a * b) + (p_5 * b^{**2}) + (p_6 * a^{**3}) + (p_7 * a^{**2} * b) + (p_8 * a * b^{**2}) + (p_9 * b^{**3}) + \dots$$

- If ND = 3

$$y = p_0 + (p_1 * a) + (p_2 * b) + (p_3 * c) + (p_4 * a^{**2}) + (p_5 * a * b) + (p_6 * a * c) + (p_7 * b^{**2}) + (p_8 * b * c) + (p_9 * c^{**2}) + (p_{10} * a^{**3}) + (p_{11} * a^{**2} * b) + (p_{12} * a^{**2} * c) + (p_{13} * a * b^{**2}) + (p_{14} * a * b * c) + (p_{15} * a * c^{**2}) + (p_{16} * b^{**3}) + (p_{17} * b^{**2} * c) + (p_{18} * b * c^{**2}) + (p_{19} * c^{**3}) + (p_{20} * a^{**4}) + \dots$$

## Examples of Polynomial Controlled Sources

$$GR = i_{17-3} = 10^{-3}(v_{10-3} + 1.5v_{10-3}^2)$$

```
GR 17 3 10 3 0 1M 1.5M
```

$$EX = v_{18} = v_{13} + v_{15} + v_{17}$$

```
EX 18 0 POLY(3) 13 0 15 0 17 0 0 1 1 1
```

$$F1 = i_{12-10} = 1mA - 1.5mAi_{VCC}$$

```
F1 12 10 VCC 1MA -1.5M
```

$$HXY = v_{13-20} = 500i_{VIN1}i_{VIN2}$$

```
HXY 13 20 POLY(2) VIN1 VIN2 0 0 0 0 500
```

## Nonlinear Controlled Sources

- Type:  $y = b(v_c, i_c)$   
where  $y$  can be a voltage or a current,  $b$  is an arbitrary function of the DC values of the controlling signals  $v_c$  and  $i_c$
- Syntax  
BXXXXXXXX N+ N- <I=EXPR> <V=EXPR>
- Available functions and operators for the expression:

abs	asinh	cosh	sin			
acos	atan	exp	sinh	+	-	*
acosh	atanh	ln	sqrt	/	^	unary -
asin	cos	log	tan			

## Examples of Nonlinear Controlled Sources

$$i_2 = \cos(v_1) + \sin(v_3)$$

$$\text{B1 } 0 \ 2 \ \text{I}=\cos(v(1))+\sin(v(3))$$

$$v_{2-3} = \ln(\cos(\log(v_{1-2}^2))) + v_3 v_1$$

$$\text{B2 } 2 \ 3 \ \text{V}=\ln(\cos(\log(v(1,2)^2)))+v(3)*v(1)$$

$$v_5 = 7e^{\pi i v_d}$$

$$\text{B3 } 5 \ 0 \ \text{V}=7*\exp(\text{pi}*i(Vd))$$

## Ejemplo: Sensor de Presión Piezoresistivo

Simular un transductor piezoeléctrico de dos terminales cuya resistencia eléctrica  $r$  depende de su estrés mecánico  $\sigma$  (presión) y de su temperatura  $T$ , según la ecuación:

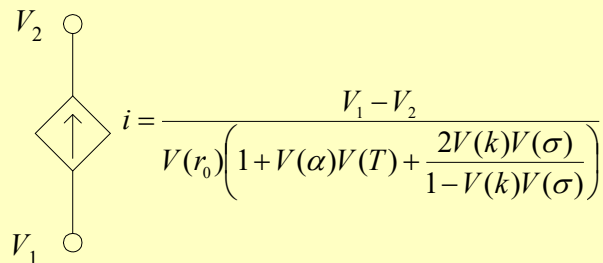
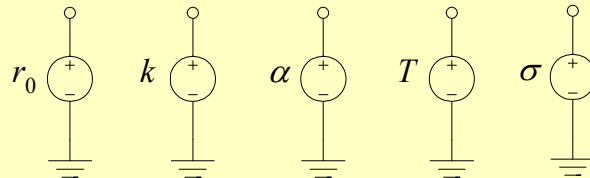
$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

$r_0$  es la resistencia del transductor a 0 grados centígrados y 0 KPa de presión ( $r_0 = 10\text{K}\Omega$ )

$\alpha$  y  $k$  son constantes conocidas ( $\alpha = 5 \times 10^{-3}$  y  $k = 0.006$ )

## Sensor de Presión Piezoresistivo

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$



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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad (r_0 = 10\text{K}\Omega, \alpha = 5 \times 10^{-3}, k = 0.006)$$

probando la ecuación...

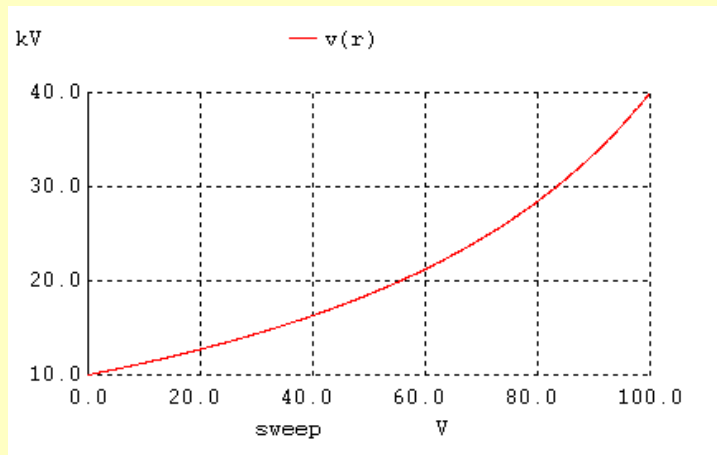
```
Strain Transducer Equation
*
vk k 0 DC 0.006
vT T 0 DC 0
valfa alpha 0 DC 5e-3
vsigma sigma 0 DC 0
vr0 r0 0 DC 10K
bp 0 r i=v(r0)*(1+v(alfa)*v(T)+2*v(k)*v(sigma)/(1-v(k)*v(sigma)))
RL r 0 1
.control
DC vsigma 0 100 0.1
plot v(r)
DC vT -40 120 0.1
plot v(r)
DC vsigma 0 100 1 vT -40 120 20
plot v(r)
.endc
.end
```

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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad r \text{ vs. } \sigma \text{ con } T = 0 \text{ } ^\circ\text{C}$$

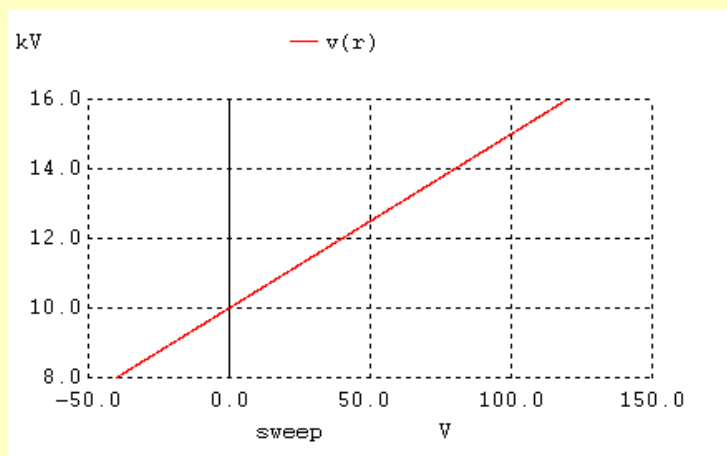


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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad r \text{ vs. } T \text{ con } \sigma = 0 \text{ KPa}$$



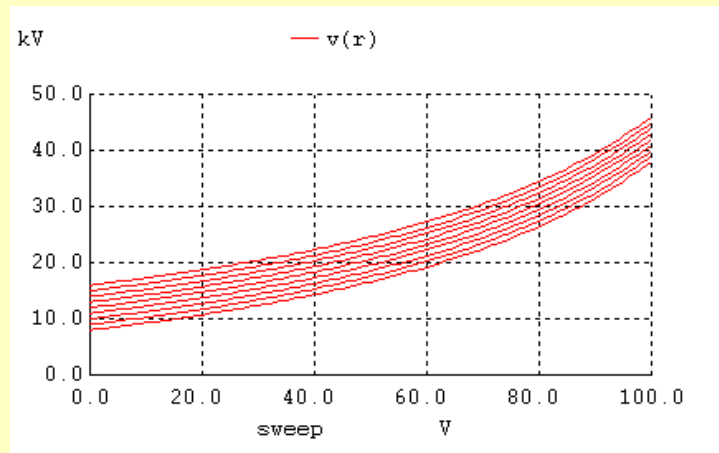
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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad r \text{ vs. } \sigma \text{ con } T: -40 \text{ a } 120 \text{ } ^\circ\text{C}$$



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## Sensor de Presión Piezoresistivo (cont)

Plotting in WinSpice with suitable text labels:

```
.control
destroy all
DC vsigma 0 100 0.1
r = v(r)
plot r xunits KPa yunits Ohms xlabel sigma
DC vT -40 120 0.1
r = v(r)
plot r xunits Celsius yunits Ohms xlabel T
DC vsigma 0 100 1 vT -40 120 20
r = v(r)
plot r xunits KPa yunits Ohms xlabel sigma
.endc
```

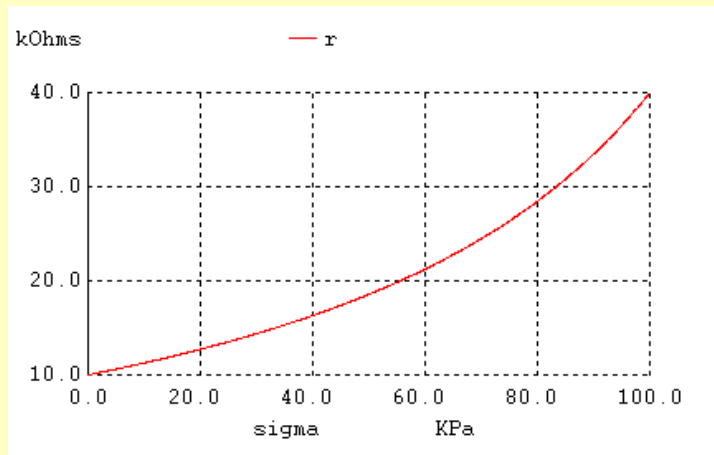
(only for WinSpice version 2004 or newer)

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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad r \text{ vs. } \sigma \text{ con } T = 0 \text{ }^\circ\text{C}$$

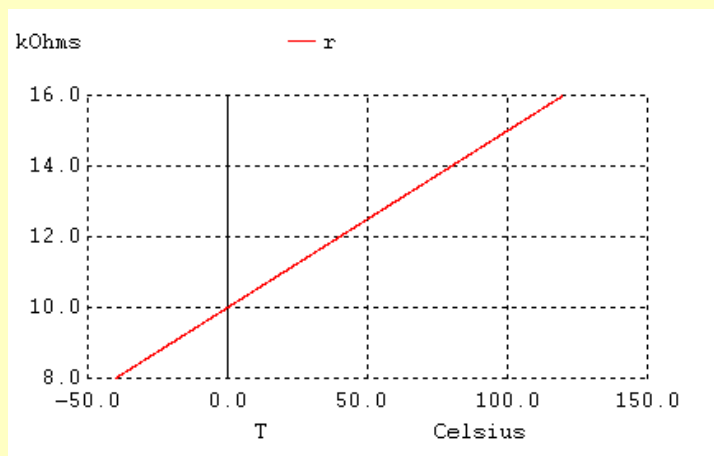


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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad r \text{ vs. } T \text{ con } \sigma = 0 \text{ KPa}$$

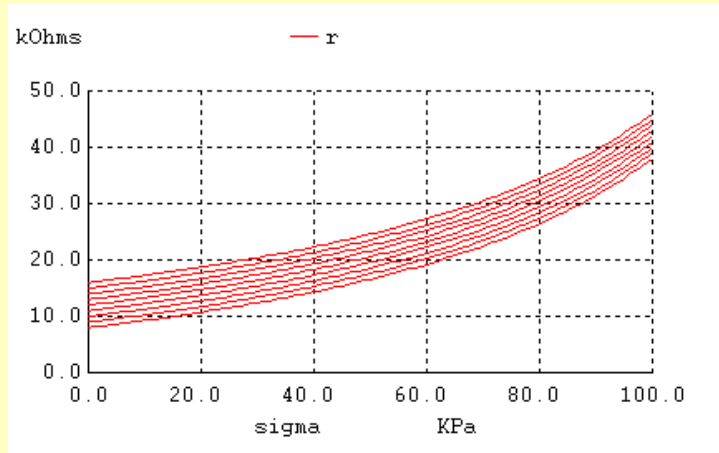


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## Sensor de Presión Piezoresistivo (cont)

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right) \quad r \text{ vs. } \sigma \text{ con } T: -40 \text{ a } 120 \text{ } ^\circ\text{C}$$

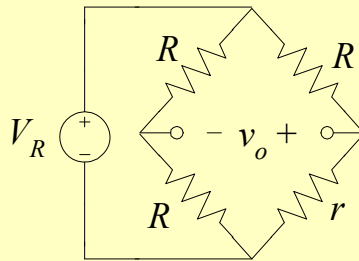


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## Usando el Sensor de Presión Piezoresistivo

$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$



$$V_R = 5V$$

$$R = 10K\Omega$$

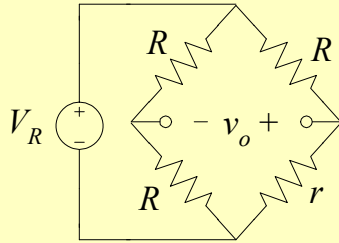
Strain Transducer in Wheatstone Bridge

```
*
VR vcc 0 5V
R1 vcc outn 10K
R2 vcc outp 10K
R3 outn 0 10K
vk k 0 DC 0.006
vT T 0 DC 0
valfa alpha 0 DC 5e-3
vsigma sigma 0 DC 0
vr0 r0 0 DC 10K
bp outp 0 i=v(outp)/(v(r0)*(1+v(alpha)*v(T)
+ +2*v(k)*v(sigma)/(1-v(k)*v(sigma))))
.control
DC vsigma 0 100 0.1
plot v(outp,outn)
DC vT -40 120 0.1
plot v(outp,outn)
DC vsigma 0 100 1 vT -40 120 20
plot v(outp,outn)
.endc
.end
```

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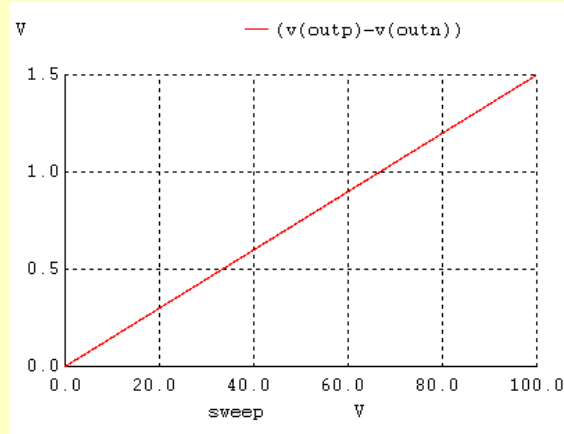
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## Usando el Sensor de Presión Piezoresistivo (cont)



$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

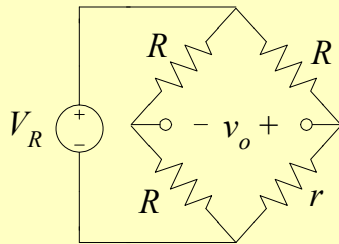
$v_o$  vs.  $\sigma$  con  $T = 0 \text{ }^\circ\text{C}$



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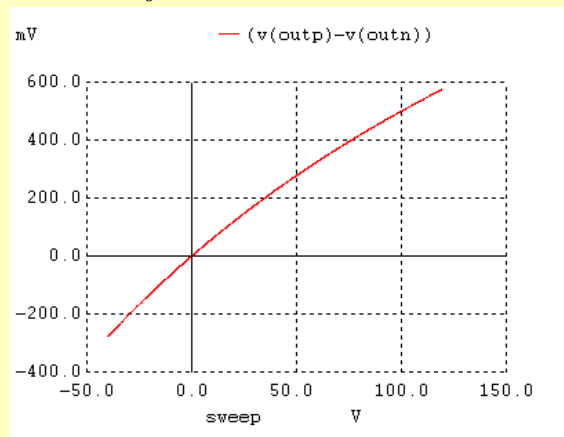
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## Usando el Sensor de Presión Piezoresistivo (cont)



$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

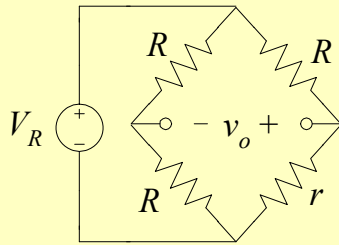
$v_o$  vs.  $T$  con  $\sigma = 0 \text{ kPa}$



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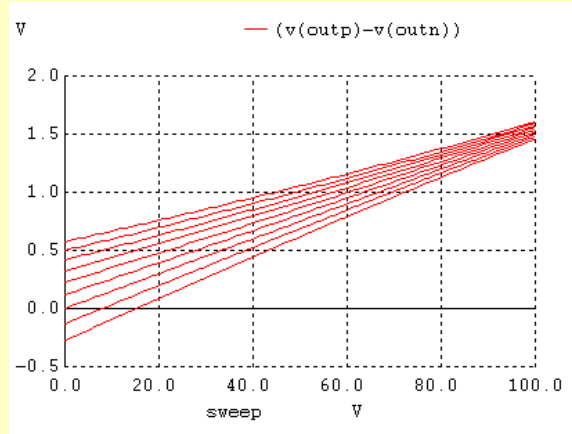
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## Usando el Sensor de Presión Piezoresistivo (cont)



$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

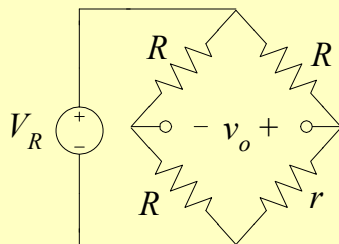
$v_o$  vs.  $\sigma$  con  $T: -40$  a  $120$  °C



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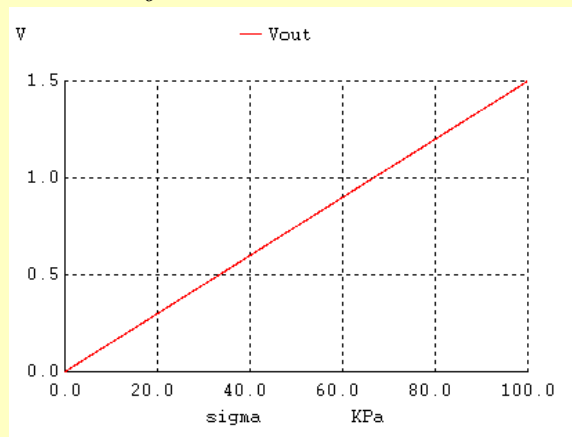
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## Usando el Sensor de Presión Piezoresistivo (cont)



$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

$v_o$  vs.  $\sigma$  con  $T = 0$  °C

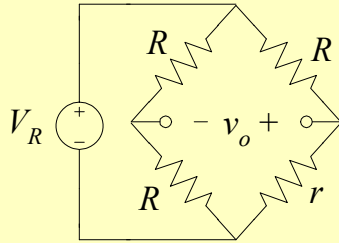


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(controlling labels and units)

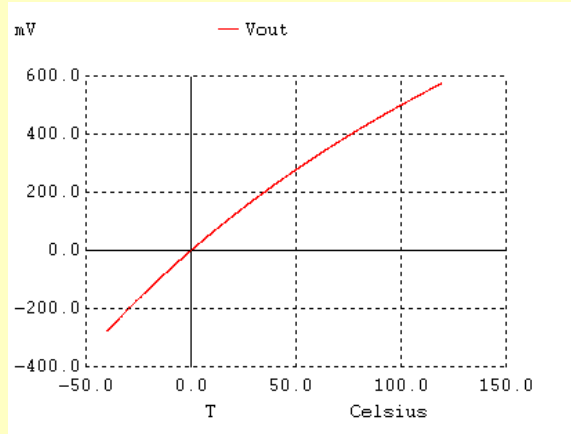
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## Usando el Sensor de Presión Piezoresistivo (cont)



$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

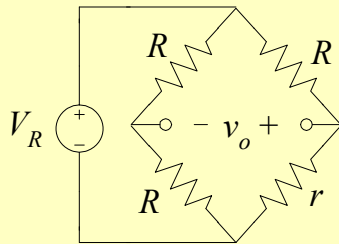
$v_o$  vs.  $T$  con  $\sigma = 0$  kPa



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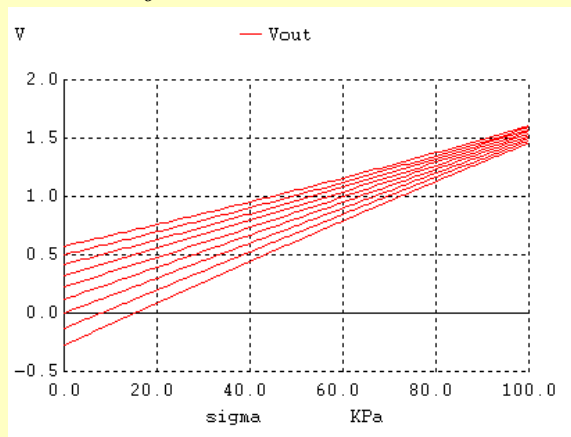
(controlling labels and units) 27

## Usando el Sensor de Presión Piezoresistivo (cont)



$$r = r_0 \left( 1 + \alpha T + \frac{2k\sigma}{1 - k\sigma} \right)$$

$v_o$  vs.  $\sigma$  con  $T : -40$  a  $120$  °C



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(controlling labels and units) 28